

Pit-Bench-Pattern #

5-15-12

BLAST HOLE

DATE:

8/14/90

Submittal Date

8-13-90 1:30 PM

Hot NaOH Shake

and

NAME:

Chad A

FIRE DETERMINATIONS

FIRE		NaOH		FIRE		NaOH	
SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	1	.022	25.	Standard ✓		.014	
2.	21	.022	26.	303 (1)			RETURN
3.	22	.018	27.	303 (2)			
4.	201	.043	28.	304		.035	
5.	221	.037	29.	305		.042	
6.	222	.062	30.	306		.026	
7.	241	.060	31.	321		.016	
8.	Standard ✓	.015	32.	322		.010	
9.	242	.022	33.				
10.	243	.046	34.				
11.	261	.030	35.	323		.050	
12.	262	.030	36.	324		.073	
13.	263	.046	37.	325		.026	
14.	264	.033	38.	326		.024	
15.	281	.080	39.	327		.029	
16.			40.	367		.023	
17.			41.	388		.006	
18.	✓6	.028	42.	Standard ✓		.015	
19.	282	.022	43.				
20.	283	.076	44.				
21.	284	.125	45.				
22.	285	.033	46.				
23.	301	.076	47.				
24.	302	.031	48.				

Pit-Bench-Pattern #

5-15-12

Submittal Date

8-14-90

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONSDATE: 8/15/90NAME: Chad A W

	FIRE		NaCN		FIRE		NaCN	
	SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	41		.026	25.	Standard ✓		.015	
2.	42		.077	26.	124(1)		.015	
3.	43		.030	27.	124(a)		.015	
4.	61		.039	28.	125		.004	
5.	62		.028	29.	141		.038	
6.	63		.019	30.	142		.077	
7.	64		.014	31.	143		.034	
8.	Standard ✓		.015	32.	144		.051	
9.	81		.016	33.				
10.	82		.009	34.				
11.	83		.019	35.	145		.015	
12.	84		.011	36.	146		.012	
13.	85		.005	37.	166		.025	
14.	101		.016	38.	387		.018	
15.	102		.016	39.	408		.007	
16.				40.	409		.010	
17.				41.	429		.009	
18.	✓6		.030	42.	Standard ✓		.015	
19.	103		.013	43.	430		.007	
20.	104		.005	44.	450		.012	
21.	105		.006	45.	451		.006	
22.	121		.019	46.	471		.023	
23.	122		.023	47.	472		.013	
24.	123		.034	48.		sta ✓	.014	

Fit-Bench-Pattern #

S-15-12

BLAST BOLE

DATE: 8/15/90

Submital Date

8-14-90

Hot NaCN Shake
and
FIRE DETERMINATIONS

NAME: Chada ✓

	FIRE	NaCN	FIRE	NaCN
	SAMPLE	Au.	SAMPLE	Au.
1.	492		Standard ✓	
2.	493			
3.	513			
4.	514			
5.	534			
6.	535			
7.	556(1)			
8.	Standard ✓			
9.	556(2)			
10.	✓6			
11.	303(1)			
12.	303(2)			
13.	A			
14.				
15.				
16.				
17.				
18.			Standard ✓	
19.				
20.				
21.				
22.				
23.				
24.				

Rerun



Pit-Bench-Pattern #

S-15-12

BLAST HOLE

DATE: 8/16/90

NAME: Choda

Submittal Date

8-15-90 1:30PM

Hot NaCN Shake
and
FIRE DETERMINATIONS

	FIRE	NaCN		FIRE	NaCN
	SAMPLE	Au.	Au.	SAMPLE	Au.
1.	161		.089	25.	Standard ✓ .014
2.	162		.087	26.	227(1) .017
3.	163		.060	27.	227(2) .019
4.	164		.028	28.	244 .067
5.	165		.047	29.	245 .119
6.	181		.029	30.	246 .044
7.	182		.086	31.	247 .026
8.	Standard ✓		.015	32.	265 .059
9.	183		.095	33.	
10.	184		.042	34.	
11.	185		.032	35.	266 .038
12.	186		.029	36.	267 .038
13.	202		.052	37.	286 .055
14.	203		.116	38.	287 .076
15.	204		.111	39.	307 .026
16.				40.	308 .042
17.				41.	328 .020
18.	V6		.026	42.	Standard ✓ .015
19.	205		.077	43.	349 .007
20.	206		.077	44.	365 .052
21.	223		.056	45.	366 .014
22.	224		.165	46.	386 .023
23.	225		.036	47.	389 .007
24.	226		.020	48.	Standard ✓ .015

Fit-Bench-Pattern #

S-15-12

Submittal Date

8-15-90 1:30 PM

BLAST HOLE

Hot NaCN Shake
and

FIRE DETERMINATIONS

DATE:

8/16/90

NAME:

Chad A W

FIRE		NaCN		FIRE		NaCN	
SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	390	.038	25.	Standard ✓		.015	
2.	407	.028	26.	494(1)		.008	
3.	410	.013	27.	494(2)		.007	
4.	411	.015	28.	512		.024	
5.	428	.005	29.	600		.003	
6.	431	.012	30.	601		.005	
7.	432	.059	31.	602		.006	
8.	Standard ✓	.015	32.	603		.008	
9.	446	.012	33.				
10.	447	.013	34.				
11.	448	.074	35.	604		.053	
12.	449	.011	36.	605		.011	
13.	452	.017	37.	606		.005	
14.	453	.015	38.	368		.046	
15.	468	.017	39.	369		.053	
16.			40.	370		.007	
17.			41.		✓std	.015	
18.	✓6	.028	42.	Standard ✓			
19.	469	.018	43.				
20.	470	.022	44.				
21.	473	.022	45.				
22.	474	.009	46.				
23.	490	.010	47.				
24.	491	.038	48.				

Bit-Bench-Pattern #
5-15-12

Submission Date
8-16-90 1:15 PM

BLAST HOLE

Hot NaCN Shake
and
FIRE DETERMINATIONS

DATE: 8/17/90

NAME: Chada W

FIRE		NaCN		FIRE		NaCN	
SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	613		.007	25.	Standard ✓	.015	
2.	614		.004	26.	634(1)	.004	
3.	615		.002	27.	634(2)	.004	
4.	616		.006	28.	635	.008	
5.	617		.022	29.	636	.006	
6.	618		.009	30.	637	.009	
7.	619		.015	31.	638	.012	
8.	Standard ✓		.014	32.	639	.015	
9.	620		.012	33.			
10.	621		.015	34.			
11.	622		.008	35.	Standard ✓	.015	
12.	623		.008	36.			
13.	624		.013	37.			
14.	625		.012	38.			
15.	626		.020	39.			
16.				40.			
17.				41.			
18.	627		.004		Standard ✓		
19.	628		.013	43.			
20.	629		.027	44.			
21.	630		.026	45.			
22.	631		.005	46.			
23.	632		.003	47.			
24.	633		.008	48.			

Hit-Bench-Pattern #
5-15-12

BLAST HOLE

DATE: 8/17/90 0/2

Submitted Date
8-16-90 1:15 PM

Hot NaCN Shake
 and
FIRE DETERMINATIONS

NAME: Chad G VD

FIRE		NaCN		FIRE		NaCN	
SAMPLE	Au.	Au.		SAMPLE	Au.	Au.	
1.	23		.021	25.	Standard ✓	.015	
2.	44		.009	26.	403(1)	.015	
3.	45		.020	27.	403(2)	.015	
4.	341		.012	28.	404	.032	
5.	342		.048	29.	405	.005	
6.	343		.074	30.	406	.041	
7.	344		.031	31.	424	.010	
8.	Standard ✓		.015	32.	425	.011	
9.	345		.032	33.			
10.	346		.090	34.			
11.	347		.017	35.	426	.017	
12.	348		.017	36.	427	.015	
13.	361		.022	37.	515	.013	
14.	362		.022	38.	536	.009	
15.	363		.042	39.	557	.007	
16.				40.	578	.005	
17.				41.	607	.005	
18.	364		.082	42.	Standard ✓	.015	
19.	381		.017	43.	608	.013	
20.	382		.013	44.	609	.077	
21.	383		.007	45.	610	.013	
22.	384		.036	46.	611	.059	
23.	385		.022	47.	612	.027	
24.	402		.024	48.	Std. ✓	.015	

S-15-13

WRJ
OK 12/21/90

CHECKED OK 9-11-90
BM

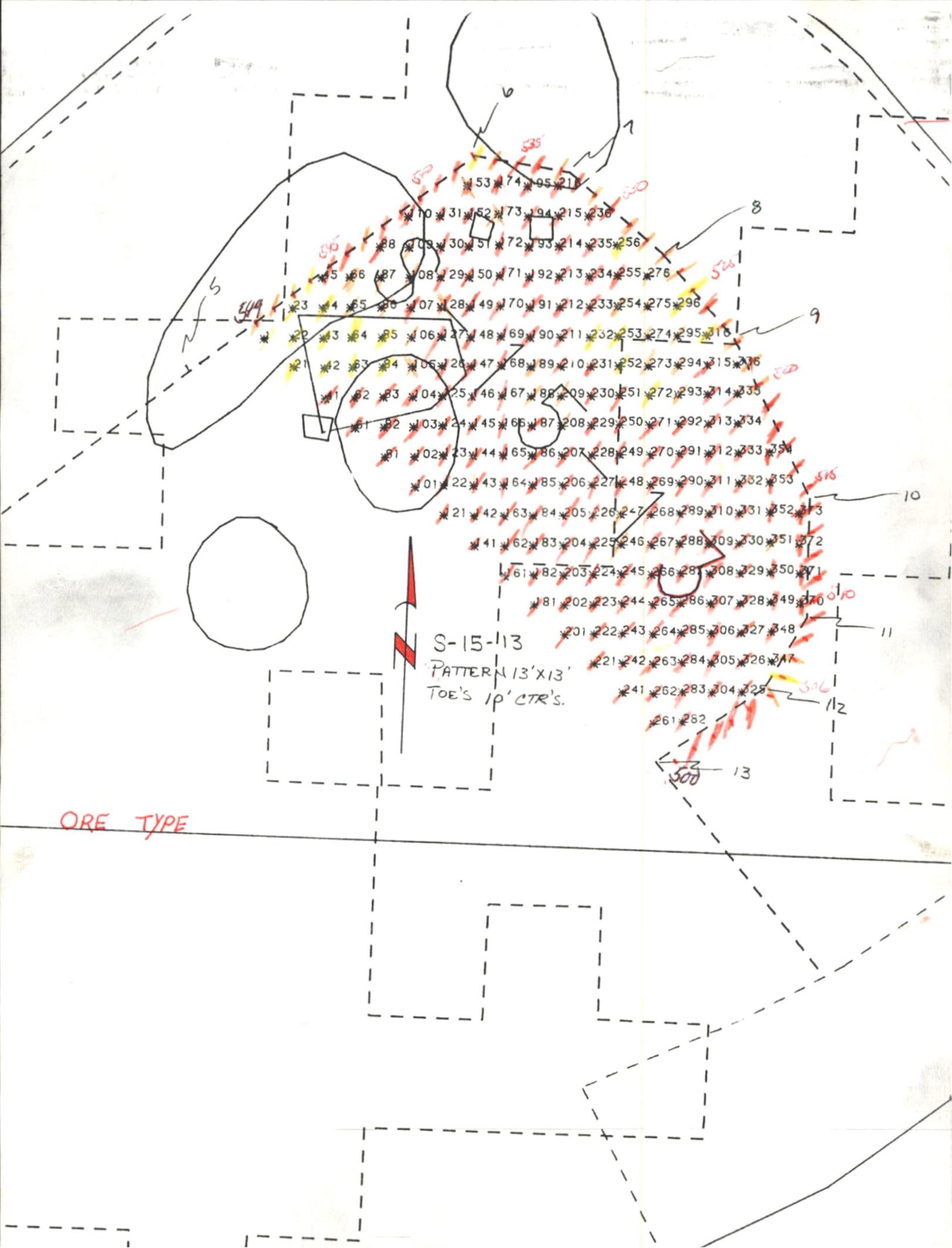
BENCH NO	SHOT NO	BLASTHOLE NO	ORE TYPE	FIRE AU	AA AU	AA/FIRE	AA/RAT
S15	13	1	1-	0.043 ✓	0.018 ✓	41.86%	0.043
S15	13	21	1-		0.019 ✓		0.020
S15	13	22	1-		0.008 ✓		0.009
S15	13	23	1-	0.035 ✓	0.033 ✓	94.29%	0.035
S15	13	41	3-	0.046 ✓	0.045 ✓	97.83%	0.046
S15	13	42	1-	0.009 ✓	0.010 ✓	111.11%	0.009
S15	13	43	1-		0.092 ✓		0.130
S15	13	44	1-	0.028 ✓	0.022 ✓	78.57%	0.028
S15	13	61	3-	0.238 ✓	0.162 ✓	68.07%	0.238
S15	13	62	3-	0.119 ✓	0.120 ✓	100.84%	0.119
S15	13	63	1-	0.021 ✓	0.019 ✓	90.48%	0.021
S15	13	64	1-		0.073 ✓		0.084
S15	13	65	2-		0.094 ✓		0.132
S15	13	66	2-		0.060 ✓		0.069
S15	13	81	3-		0.059 ✓		0.066
S15	13	82	3-		0.038 ✓		0.043
S15	13	83	3-		0.062 ✓		0.071
S15	13	84	1-	0.020 ✓	0.017 ✓	85.00%	0.020
S15	13	85	1-		0.026 ✓		0.028
S15	13	86	2-		0.063 ✓		0.072
S15	13	87	2-		0.054 ✓		0.061
S15	13	88	3-	0.164 ✓	0.150 ✓	91.46%	0.164
S15	13	101	3-	0.057 ✓	0.056 ✓	98.25%	0.057
S15	13	102	3-	0.010 ✓	0.010 ✓	100.00%	0.010
S15	13	103	3-		0.014 ✓		0.015
S15	13	104	3-	0.041 ✓	0.038 ✓	92.68%	0.041
S15	13	105	2-	0.018 ✓	0.016 ✓	88.89%	0.018
S15	13	106	2-		0.017 ✓		0.018
S15	13	107	3-		0.046 ✓		0.052
S15	13	108	2-		0.032 ✓		0.036
S15	13	109	2-		0.059 ✓		0.066
S15	13	110	3-		0.043 ✓		0.048
S15	13	121	3-		0.015 ✓		0.016
S15	13	122	3-	0.022 ✓	0.016 ✓	72.73%	0.022
S15	13	123	3-		0.015 ✓		0.016
S15	13	124	3-		0.016 ✓		0.017
S15	13	125	3-	0.130 ✓	0.123 ✓	94.62%	0.130
S15	13	126	3-	0.017 ✓	0.018 ✓	105.88%	0.017
S15	13	127	3-		0.015 ✓		0.016
S15	13	128	2-	0.065 ✓	0.066 ✓	101.54%	0.065
S15	13	129	3-	<i>No DATA</i>			
S15	13	130	3-	0.111 ✓	0.103 ✓	92.79%	0.111
S15	13	131	3-		0.021 ✓		0.022
S15	13	141	3-		0.019 ✓		0.020
S15	13	142	3-		0.012 ✓		0.013
S15	13	143	3-		0.007 ✓		0.008
S15	13	144	3-		0.016 ✓		0.017
S15	13	145	3-		0.012 ✓		0.013
S15	13	146	3-		0.023 ✓		0.024
S15	13	147	3-	0.018 ✓	0.019 ✓	105.56%	0.018
S15	13	148	3-		0.023 ✓		0.024
S15	13	149	3-	0.072 ✓	0.069 ✓	95.83%	0.072
S15	13	150	3-		0.059 ✓		0.066
S15	13	151	3-	0.043 ✓	0.042 ✓	97.67%	0.043

S15	13	152	3		0.018		0.019
S15	13	153	2	0.036	0.032	88.89%	0.036
S15	13	161	3		0.009		0.010
S15	13	162	3		0.012		0.013
S15	13	163	3	0.010	0.010	100.00%	0.010
S15	13	164	3		0.012		0.013
S15	13	165	3		0.021		0.022
S15	13	166	3	0.039	0.040	102.56%	0.039
S15	13	167	3		0.018		0.019
S15	13	168	3		0.011		0.012
S15	13	169	3		0.025		0.027
S15	13	170	3		0.028		0.030
S15	13	171	3		0.071		0.082
S15	13	172	3		0.015		0.016
S15	13	173	2	0.016	0.013	81.25%	0.016
S15	13	174	3		0.042		0.047
S15	13	181	3	0.036	0.036	100.00%	0.036
S15	13	182	3	0.007	0.005	71.43%	0.007
S15	13	183	3		0.005		0.005
S15	13	184	3		0.003		0.003
S15	13	185	3		0.012		0.013
S15	13	186	3		0.026		0.028
S15	13	187	3	0.047	0.044	93.62%	0.047
S15	13	188	2	0.013	0.011	84.62%	0.013
S15	13	189	2		0.018		0.019
S15	13	190	3		0.038		0.043
S15	13	191	3		0.055		0.062
S15	13	192	3		0.026		0.028
S15	13	193	3		0.048		0.054
S15	13	194	3	0.025	0.026	104.00%	0.025
S15	13	195	3		0.022		0.023
S15	13	201	3		0.008		0.009
S15	13	202	3		0.007		0.008
S15	13	203	3		0.005		0.005
S15	13	204	3		0.010		0.011
S15	13	205	3		0.010		0.011
S15	13	206	3		0.009		0.010
S15	13	207	3		0.016		0.017
S15	13	208	2		0.021		0.022
S15	13	209	2		0.033		0.037
S15	13	210	3	0.063	0.063	100.00%	0.063
S15	13	211	3		0.008		0.009
S15	13	212	3		0.021		0.022
S15	13	213	3		0.009		0.010
S15	13	214	3	0.005	0.005	100.00%	0.005
S15	13	215	3		0.032		0.036
S15	13	216	3		0.031		0.035
S15	13	221	3		0.008		0.009
S15	13	222	3		0.009		0.010
S15	13	223	3	0.020	0.019	95.00%	0.020
S15	13	224	3		0.030		0.034
S15	13	225	3		0.011		0.012
S15	13	226	3	0.008	0.008	100.00%	0.008
S15	13	227	3		0.012		0.013
S15	13	228	3		0.030		0.034
S15	13	229	3	0.107	0.103	96.26%	0.107

S15	13	230	3		0.032		0.036
S15	13	231	3		0.038		0.043
S15	13	232	1		0.012		0.013
S15	13	233	3		0.010		0.011
S15	13	234	3		0.018		0.019
S15	13	235	3		0.038		0.043
S15	13	236	3		0.013		0.014
S15	13	241	3		0.004		0.004
S15	13	242	3		0.009		0.010
S15	13	243	3		0.006		0.007
S15	13	244	3		0.021		0.022
S15	13	245	3		0.007		0.008
S15	13	246	2		0.014		0.015
S15	13	247	2		0.007		0.008
S15	13	248	3	0.027	0.028	103.70%	0.027
S15	13	249	3	0.018	0.019	105.56%	0.018
S15	13	250	3		0.012		0.013
S15	13	251	3		0.013		0.014
S15	13	252	1		0.004		0.004
S15	13	253	1		0.005		0.005
S15	13	254	2		0.030		0.034
S15	13	255	3	0.171	0.164	95.91%	0.171
S15	13	256	1		0.012		0.013
S15	13	261	3		0.004		0.004
S15	13	262	3		0.006		0.007
S15	13	263	3		0.003		0.003
S15	13	264	3	0.013	0.014	107.69%	0.013
S15	13	265	3		0.019		0.020
S15	13	266	3		0.031		0.035
S15	13	267	3	0.021	0.020	95.24%	0.021
S15	13	268	3		0.021		0.022
S15	13	269	3		0.017		0.018
S15	13	270	3		0.013		0.014
S15	13	271	3		0.016		0.017
S15	13	272	1	0.018	0.019	105.56%	0.018
S15	13	273	2		0.026		0.028
S15	13	274	2	0.034	0.033	97.06%	0.034
S15	13	275	2		0.063		0.072
S15	13	276	2		0.037		0.042
S15	13	282	3		0.008		0.009
S15	13	283	3		0.003		0.003
S15	13	284	3		0.006		0.007
S15	13	285	3		0.006		0.007
S15	13	286	3		0.009		0.010
S15	13	287	3		0.012		0.013
S15	13	288	3	0.042	0.040	95.24%	0.042
S15	13	289	3	0.020	0.019	95.00%	0.020
S15	13	290	3		0.025		0.027
S15	13	291	3		0.026		0.028
S15	13	292	3		0.024		0.026
S15	13	293	2		0.034		0.038
S15	13	294	2		0.043		0.048
S15	13	295	2		0.062		0.071
S15	13	296	1		0.022		0.023
S15	13	304	3	0.037	0.036	97.30%	0.037
S15	13	305	3	0.034	0.032	94.12%	0.034

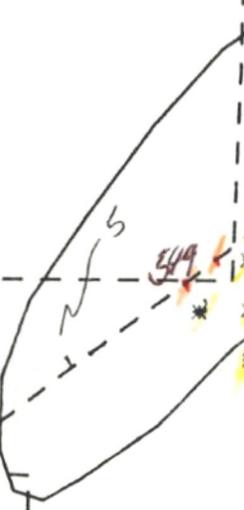
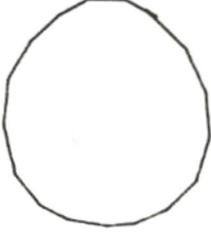
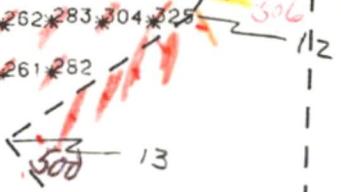
S15	13	306	3	0.011	0.010	90.91%	0.011
S15	13	307	3		0.007		0.008
S15	13	308	3		0.014		0.015
S15	13	309	3		0.012		0.013
S15	13	310	3	0.016	0.016	100.00%	0.016
S15	13	311	3		0.010		0.011
S15	13	312	3		0.007		0.008
S15	13	313	3	0.064	0.062	96.88%	0.064
S15	13	314	3	0.021	0.020	95.24%	0.021
S15	13	315	3		0.032		0.036
S15	13	316	1		0.023		0.024
S15	13	325	3	0.099	0.095	95.96%	0.099
S15	13	326	3		0.008		0.009
S15	13	327	3		0.017		0.018
S15	13	328	3		0.008		0.009
S15	13	329	3	0.010	0.008	80.00%	0.010
S15	13	330	3		0.006		0.007
S15	13	331	3		0.004		0.004
S15	13	332	3		0.009		0.010
S15	13	333	3		0.013		0.014
S15	13	334	3	0.051	0.050	98.04%	0.051
S15	13	335	3		0.011		0.012
S15	13	336	2		0.016		0.017
S15	13	348	3		0.004		0.004
S15	13	349	3		0.007		0.008
S15	13	350	3	0.007	0.005	71.43%	0.007
S15	13	351	3		0.006		0.007
S15	13	352	3		0.006		0.007
S15	13	353	3		0.011		0.012
S15	13	354	3		0.009		0.010
S15	13	370	3		0.007		0.008
S15	13	371	3		0.006		0.007
S15	13	372	3		0.012		0.013
S15	13	373	3		0.007		0.008
S15	13	501	3		0.020		0.021
S15	13	502	3		0.021		0.022
S15	13	503	3		0.007		0.008
S15	13	504	3	0.009	0.006	66.67%	0.009
S15	13	505	2		0.005		0.005
S15	13	506	1		0.006		0.007
S15	13	507	2		0.014		0.015
S15	13	508	3	0.006	0.007	116.67%	0.006
S15	13	509	3		0.007		0.008
S15	13	510	3		0.010		0.011
S15	13	511	3		0.004		0.004
S15	13	512	3		0.006		0.007
S15	13	513	3		0.005		0.005
S15	13	514	3		0.006		0.007
S15	13	515	3		0.010		0.011
S15	13	516	3		0.009		0.010
S15	13	517	3		0.009		0.010
S15	13	518	3	0.005	0.004	80.00%	0.005
S15	13	519	3	0.022	0.020	90.91%	0.022
S15	13	520	2	0.016	0.015	93.75%	0.016
S15	13	521	2	0.024	0.021	87.50%	0.024
S15	13	522	2		0.039		0.044

S15	13	523	2		0.019		0.020
S15	13	524	3		0.028		0.030
S15	13	525	1	0.014	0.013	92.86%	0.014
S15	13	526	2		0.027		0.029
S15	13	527	2		0.025		0.027
S15	13	528	2		0.024		0.026
S15	13	529	2		0.009		0.010
S15	13	530	3		0.031		0.035
S15	13	531	2	0.024	0.023	95.83%	0.024
S15	13	532	3		0.082		0.115
S15	13	533	2	0.301	0.269	89.37%	0.301
S15	13	534	3		0.047		0.053
S15	13	535	3		0.029		0.031
S15	13	536	2	0.045	0.043	95.56%	0.045
S15	13	537	1		0.067		0.077
S15	13	538	3		0.022		0.023
S15	13	539	3		0.026		0.028
S15	13	540	3		0.025		0.027
S15	13	541	3	0.023	0.021	91.30%	0.023
S15	13	542	3		0.042		0.047
S15	13	543	2		0.025		0.027
S15	13	544	3		0.020		0.021
S15	13	545	3	0.019	0.020	105.26%	0.019
S15	13	546	1		0.022		0.023
S15	13	547	1		0.015		0.016
S15	13	548	2	0.039	0.038	97.44%	0.039
S15	13	549	2		0.016		0.017
		MEAN		0.044	0.027	93.35%	0.030



S-15-13
 PATTERN 13'X13'
 TOE'S 10' CTR'S.

ORE TYPE



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